A. Huang, J. M. A. Tanskanen, and I. O. Hartimo, "Design of optimum power estimator based on Wiener model applied to mobile transmitter power control," in *Proc. of 1998 IEEE International Symposium on Circuits and Systems*, Monterey, California, USA, May 1998, pp. 249–252.

DESIGN OF OPTIMUM POWER ESTIMATOR BASED ON WIENER MODEL APPLIED TO MOBILE TRANSMITTER POWER CONTROL

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ABSTRACT

Estimation of signal power/instantaneous energy requires nonlinear systems. A power estimator based on the Wiener model is proposed in this paper. Its input signal can be complex-valued, e.g., a baseband signal in a communications system, and its output is guaranteed to be positive. It is computationally very efficient as compared to quadratic filters, and allows for a predescribed prediction step required, for example, for application in delay sensitive closed control loops. Two methods of optimum/partial-optimum design are presented. The partially-optimized power estimator is simulated in COSSAP environment as a part of the power control loop of a CDMA mobile radio communication system. The system performance improvements are observed from bit error rate reductions.

1. INTRODUCTION

Power (instantaneous energy) of a signal is defined as the square of the signal magnitude, i.e., $|x(t)|^2$ at a continuous time instant *t*, or $|x(n)|^2$ at a discrete time instant *n*. A standard power estimator for real-valued signals, which is also called standard energy detector, consists of a linear time invariant (LTI) filter followed by a magnitude-square operation [1]. A more general power estimation system for real-valued signals is referred to as quadratic filter (QF) or a quadratic detector [1][2]. QF can provide better trade-off between different desired features [2]. However, the large processing delay and the heavy computational requirements of quadratic filtering precludes its real-time use. Moreover, the resulting power estimate is not guaranteed to be positive.

In engineering, computationally efficient power estimation of complex-valued signals is often needed. For example, it is very important to keep the signal powers received at a base station from all the mobile users in a mobile CDMA radio communications system at equal and constant level by controlling their transmitted powers [3][4]. The powers of the received noisy baseband signals should be measured, filtered and compared with a preset power level threshold, so that power control can be realized by a control loop, and the mutual interference between different users can be reduced. The use of a predictive power estimator in the power control loop has been suggested to improve the performance of mobile radio communication systems [5][6]. The function of the predictive power estimator is threefold: to reduce additive noise and corrupting interference (i.e., filtering), to calculate the received signal power level which is affected by channel fading and the distance between the mobile handset and the base station (i.e., measuring), and to predict the future value of the power of the received signal. Predictive power estimator reduces to power measurement if its filtering/prediction function is removed. The power estimator has to be computationally efficient to be applied in real²Inst. of Detection Tech. & Intelligent Instrument Dept. of Scientific Instrument, Zhejiang Univ. Hangzhou 310027, China

time control.

In this paper we propose a power estimator (PE) for complex-valued signals, with an application in the power control loop in CDMA mobile radio systems. This PE has a structure based on the Wiener model [1][2][7][8] and it is thus computationally very efficient. It can be designed to be predictive. Also, the output is guaranteed to be positive as required by the power estimation applications. In Section II, the structure is presented and discussed. Two methods of optimum design are derived in Section III, and the partially-optimized PE is demonstrated with a simple example. The results of communication system simulations in COSSAP environment are given in Section IV. Section V concludes the paper.

2. POWER ESTIMATOR BASED ON WIENER MODEL

The *Wiener model* (WM) consists of a FIR filter followed by a squaring operation [1][2]. It has been called the standard energy detector for real-valued signals because its structure reflects the function of removing noise and then calculating signal power. It can be viewed as a QF with a dyadic kernel, or a special case of the Wiener system used for nonlinear system recognition [1][2][7][8]. It is of practical interest due to its simple structure.

For complex-valued signals, we construct a PE with two WMs and an adder (Fig. 1). The output of the system is estimated *power* of the input signal, rather than an estimate of the input signal itself. The difficulties in derivation and analysis are inherent due to nonlinearity. The two FIR filters are usually chosen to be equal according to the assumptions on the input which will be addressed later. They have a real impulse response h(n), and are designed off-line according to the characteristics of the input.



Figure 1. The power estimator for complex-valued signals.

Input is a sum of the received signal and corrupting noise, both of which are complex. The signal $x(n)=x_R(n)+jx_I(n)$ is assumed to be a wide-sense stationary process with known statistics. Its real part and imaginary part are uncorrelated and normally have *equal statistics*. The real part $w_R(n)$ and imaginary part $w_I(n)$ of the corrupting noise w(n) are assumed to be uncorrelated, both are white Gaussian noise (WGN) with zero mean, equal variance $\sigma_w^2/2$ and

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kurtosis 3 $\sigma_w^4/4$ [9]. Hence, w(n) is an additive WGN process with zero mean, variance σ_w^2 and kurtosis 2 σ_w^4 (see Appendix 1). For the optimum PE formulation, we define input signal-to-noise ratio (SNR) as the ratio of average powers of input *signal* and *corrupting noise*

$$\gamma = E\{|x(n)|^2\} / E\{|w(n)|^2\} = R_x(0) / \sigma_w^2$$
(1)

where $E\{\cdot\}$ denotes the expectation, $R_x(l)$ is the autocorrelation function whose value at the origin is the average power $R_x(0)$ of the signal.

The output $y(n)=|x(n+p)|^2+e(n)$ is an estimate of the signal power $|x(n)|^2=x_R^2(n)+x_I^2(n)$ with a prediction step *p*. The value of *p* can be any integer depending on the underlying application. For instance, p>0 refers to a *p*-step-ahead power prediction. The mean value of the *desired output* $|x(n+p)|^2$ can be obtained according to the stationary characteristics of x(n), as

$$E\{|x(n+p)|^2\} = E\{|x(n)|^2\} = R_x(0).$$
(2)

The output y(n) can also be expressed in terms of the filtered input r(n) as

$$y(n) = |r(n)|^2 = r(n)r^*(n) = \mathbf{h}^{\mathrm{T}}(\mathbf{x} + \mathbf{w})(\mathbf{x} + \mathbf{w})^{*\mathrm{T}}\mathbf{h}$$
(3)

where $r(n) = r_R(n)+jr_I(n) = \mathbf{h}^T(\mathbf{x}+\mathbf{w})$ with the length-*N* filter impulse response vector $\mathbf{h} = [h(0) \dots h(N-1)]^T$, the signal vector $\mathbf{x} = [x(n) \dots x(n-N+1)]^T$, and the noise vector $\mathbf{w} = [w(n) \dots w(n-N+1)]^T$, the superscript "*" denotes complex conjugate, and "T" denotes transpose. y(n) is always positive due to the squaring operation.

The real-valued power estimation error is defined as the difference between the practical output and the desired output

$$e(n) = y(n) - |x(n+p)|^2 = r(n)r^*(n) - x(n+p)x^*(n+p).$$
(4)

This error consists of the second-order terms $x^2(n)$ and $w^2(n)$, as well as the cross term of x(n) and w(n). That is, this error is both signal-dependent and noise-dependent after the nonlinear operation. The estimation bias, i.e., the mean of e(n), can be derived as

$$Bias = E\{e(n)\} = \mathbf{h}^{\mathrm{T}} \mathbf{R}_{x} \mathbf{h} + \sigma_{w}^{2} G_{n} - R_{x}(0)$$
(5)

where $\mathbf{R}_{\mathbf{x}} = E\{\mathbf{x}\mathbf{x}^{*^{\mathrm{T}}}\}\$ is the autocorrelation matrix of the signal, and $G_n = \mathbf{h}^{\mathrm{T}}\mathbf{h}$ is the noise gain of the filter. This bias is unavoidable because of the existence of the second-order terms in the expression of e(n). The estimation variance, i.e., mean squared error (MSE), can be expressed as

$$E\{e^{2}(n)\} = E\{y^{2}(n)\} - 2E\{y(n)|x(n+p)|^{2}\} + E\{|x(n+p)|^{4}\}.$$
 (6)

In the following text, both the terms "MSE" and "variance" are used depending on the context.

3. OPTIMUM DESIGN

There are two methods to optimize the PE based on WM, as derived in the following.

3.1 Global Optimization and Numerical Solution

The global optimization is performed to design the FIR filters to minimize the MSE $E\{e^2(n)\}$ at the output of the PE. Taking the partial derivative of (6) with respect to **h** yields (see Appendix 2)

$$\frac{\partial E\{e^2(n)\}}{\partial \mathbf{h}} = 2E\{(\mathbf{S} + \mathbf{S}^*)\mathbf{h}\mathbf{h}^T\mathbf{S}\}\mathbf{h} - 2E\{|x(n+p)|^2(\mathbf{S} + \mathbf{S}^*)\}\mathbf{h}$$
(7)

where $\mathbf{S} = (\mathbf{x}+\mathbf{w})(\mathbf{x}+\mathbf{w})^{*^{T}}$ is an *N*×*N* Hermitian matrix. Noting that **h** is a non-zero vector, we set the partial derivative in (7) to zero, eliminate **h** from both terms, and obtain

$$E\{(\mathbf{S} + \mathbf{S}^*)\mathbf{h}_G \mathbf{h}_G^T \mathbf{S}\} = E\{|x(n+p)|^2 \cdot (\mathbf{S} + \mathbf{S}^*)\}$$
(8)

where the subscript "*G*" denotes global optimization. Equation (8) can not be further simplified due to the existence of the expectations. It provides an implicit expression for iteratively calculating the optimal filter impulse response \mathbf{h}_G for a globally-optimized PE. However, the numerical calculations could be massive and possess some uncertainty in the obtained \mathbf{h}_G , and also convergence is not guaranteed.

3.2 Partial Optimization and Analytical Solution

As the globally-optimal solution is difficult to obtain, we turn to seek a partially-optimal solution. Let the filtered input signal in Fig. 1 be expressed as $r(n)=x(n+p)+\varepsilon(n)$ where $\varepsilon(n)=\varepsilon_R(n)+j\varepsilon_l(n)$ is the estimation error at the output of the FIR filters (Fig. 2). The goal is to minimize the MSE $E\{|\varepsilon(n)|^2\} = E\{\varepsilon_R^2(n)\} + E\{\varepsilon_l^2(n)\}$ so that an optimal estimate of *the delayed signal* is achieved at the output of *the filters*, and the MSE $E\{e^2(n)\}$ at the PE output is in turn reduced. That is, the overall PE is to be partially optimized.



Figure 2. The Wiener model processing the real part of the input.

First, the WM which processes the real part of the input (Fig. 2) is considered. The optimal filter minimizing $E\{\varepsilon_R^2(n)\}$ is actually the Wiener filter whose impulse response can be calculated from the Wiener-Hopf equation [10] as

$$\mathbf{h}_{opt} = \mathbf{R}_{R}^{-1} \mathbf{r}_{R} \tag{9}$$

where $\mathbf{R}_R = E\{(\mathbf{x}_R + \mathbf{w}_R)(\mathbf{x}_R + \mathbf{w}_R)^{\mathrm{T}}\}\$ is an $N \times N$ auto-correlation matrix, $\mathbf{r}_R = E\{x_R(n+p)[\mathbf{x}_R + \mathbf{w}_R]\}\$ is a cross-correlation vector, and \mathbf{x}_R and \mathbf{w}_R are the real parts of \mathbf{x} and \mathbf{w} respectively. The optimal filter impulse response \mathbf{h}_{opt} is thus real-valued. Noting that $w_R(n)$ is zero-mean WGN with a variance of $\sigma_w^2/2$, and that it is independent of $x_R(n)$, further derivation yields $\mathbf{r}_R = E\{x_R(n+p)\mathbf{x}_R\}\$ and $\mathbf{R}_R = E\{\mathbf{x}_R\mathbf{x}_R^{\mathrm{T}}\} + \sigma_w^2\mathbf{I}/2$. Letting $\mathbf{r}_{xR} = E\{x_R(n+p)\mathbf{x}_R\}\$ and $\mathbf{R}_{xR} = E\{\mathbf{x}_R\mathbf{x}_R^{\mathrm{T}}\}$, the Wiener-Hopf equation can be further elaborated as

$$\mathbf{h}_{opt} = (\mathbf{R}_{xR} + \sigma_w^2 \mathbf{I}/2)^{-1} \mathbf{r}_{xR} \,. \tag{10}$$

Correspondingly, the minimum MSE (MMSE) achieved at the output of the Wiener filter is [10]

$$E\{\varepsilon_R^2(n)\}_{\min} = R_x(0)/2 - \mathbf{r}_{xR}^T \mathbf{h}_{opt}.$$
 (11)

Secondly, we consider the optimization of the WM which processes the imaginary part of the input. It has been assumed that the real and the imaginary parts of the signal have equal statistics, and so do the real and the imaginary parts of the noise. Therefore, the optimal filter impulse response in this WM must be also \mathbf{h}_{opt} , and the MMSE $E\{ \varepsilon_l^2(n) \}_{min}$ at the filter output equals to $E\{ \varepsilon_R^2(n) \}_{min}$. Hence, the partially-optimized PE consists of an adder and two WMs with equal Wiener filters. The power estimation bias in (5) A. Huang, J. M. A. Tanskanen, and I. O. Hartimo, "Design of optimum power estimator based on Wiener model applied to mobile transmitter power control," in *Proc. of 1998 IEEE International Symposium on Circuits and Systems*, Monterey, California, USA, May 1998, pp. 249– 252.

can be expressed now in terms of the MMSE $E\{|\varepsilon(n)|^2\}_{min}$ at the Wiener filters' outputs as (see Appendix 3)

$$Bias_{\min} = -E\{|\varepsilon(n)|^2\}_{\min} = -2 E\{\varepsilon_R^2(n)\}_{\min}.$$
 (12)

The variance in (6) can also be further derived, although its general expression is long and not given here.

A simple case is studied to illustrate the partial optimum solution. The input signal is chosen to be a constant which is an approximation of narrow-band fading signals. We set $x(n) = X_R + jX_I = X_R(1+j)$ to satisfy the assumption on equal statistics. Hence, $R_x(0)=2 X_R^2$, $\mathbf{R}_{xR}=X_R^2 \mathbf{E}$ and $\mathbf{r}_{xR}=X_R^2 \mathbf{e}$. Here \mathbf{E} is an $N \times N$ matrix with all the elements of unity, and \mathbf{e} is a length-N vector with all the elements of unity. Substituting these into (10), the impulse response of the Wiener filter can be obtained in terms of the input SNR and the filter length, as

$$\mathbf{h}_{opt} = \mathbf{e}\gamma / (1 + N\gamma) = b\mathbf{e} \ . \tag{13}$$

where the coefficient value $b = \gamma/(1+N\gamma)$. This closed-form expression can be used as a basis of the adaptive implementation of the partially-optimized PE [6]. The corresponding power estimation bias can be derived from (11) and (12) as

$$Bias_{\min} = -\sigma_w^2 b , \qquad (14)$$

and the variance can be derived from (6) as [6]

$$E\{e^{2}(n)\}_{\min} = \sigma_{w}^{4}\gamma^{2}(1+2N\gamma+2N^{2}\gamma^{2}+2N^{3}\gamma^{3})/(1+N\gamma)^{4}.(15)$$

For the sake of performance comparison, conventional averagers are employed since they have extremely narrow bandwidth and thus are very efficient for removing noise from constant signals. The impulse response of a conventional averager is $\mathbf{h}_{ave} = \mathbf{e}/N$ with a constant coefficient value 1/N. When it is used to construct a PE for a constant input signal in noise, the resulted power estimation bias and variance can be derived from (5) and (6), respectively, as [6]

$$Bias_{ave} = \sigma_w^2 / N$$
, and $E\{e^2(n)\}_{ave} = 2\sigma_w^4 (1 + N\gamma) / N^2$. (16)

The comparison results are depicted in Figs. 3, 4, and 5. It is observed from (13) that the Wiener filter for a constant signal in noise is a *scaled averager* which has as narrow bandwidth as that of conventional averager with the same length. Hence, it is also very efficient for noise reduction from constant signals. All the coefficient values are equal to *b* which is a function of input SNR and filter length. The maximum value of *b* is 1/N. As input SNR decreases, *b* decreases whereas the coefficient value of conventional averager stays at 1/N (Fig. 3). This feature of the Wiener filter reduces efficiently the power estimation bias and variance, as seen from Figs. 4 and 5, or by comparing (14) and (15) with (16).

4. SYSTEM SIMULATIONS

To assess the applicability of the partially-optimized PE to the power control in CDMA communication systems, a single-user simulator with a closed power control loop is constructed in COSSAP software environment. The system parameters are selected as carrier frequency 1.8 GHz, chip rate 1.2288 MHz, bit rate 9600 Hz, control period 0.625 seconds, and single bit power control command with ± 1 dB mobile transmitter power level change step. These parameters are derived from those for the Qualcomm CDMA system [11] except that the control rate



Figure 3. The Wiener filters' coefficient values *b* for constant signals, and the coefficient values of averagers of the same lengths.



Figure 4. The estimation variances achieved by the PEs with Wiener filters and the PEs with averagers.



Figure 5. The biases achieved by the PEs with Wiener filters (the absolute value of that in (16)) and by the PEs with averagers.

is doubled. To evaluate system performance, bit error rates (BERs) are counted by comparing 100,000 bits of the received signal and the transmitted signal. Two Rayleigh fading channels are employed with maximum Doppler shifts corresponding to mobile speeds of 10 km/h and 30 km/h. Three power controllers are tested: Controller 1 using a partially-optimized one-step-ahead predictive PE (N=15), Controller 2 using a PE whose FIR filters are first degree one-step-ahead Heinonen-Neuvo (H-N) polynomial predictors [12] (N=15), and Controller 3 using power measurement (no filtering/prediction). The latter two controllers are chosen for comparisons.

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Some of the simulation results are listed in Table 1. When input SNR is 0 dB, the BER obtained by using Controller 3 is as high as 0.1284 which is not acceptable. By using Controllers 1 and 2, lower BERs are obtained as 0.0374 and 0.0524, respectively. When input SNR is 10 dB, all the controllers are able to track the actual fading channel, with a little different performances. When input SNR is as high as 20 dB, the effect of background noise and the interference on the received signal is very small and thus can be omitted. Hence, the BERs obtained by using all the three Controllers are almost equal. Similar observations can be made in the case of mobile speed 10 km/h. It is clearly seen that the controllers with predictive PEs give better performances than the controller with power measurement, especially when input SNR is low. The improvements come from the noise reduction and prediction realized by the PEs. The controller employing the partially-optimized predictive PE behaves even better than the controller using the PE with H-N predictors.

Table 1. Bit error rates under mobile speed 30 km/h.

Input SNR	0 dB	10 dB	20 dB
Controller 1	0.0374	0.0118	0.0079
Controller 2	0.0524	0.0120	0.0079
Controller 3	0.1284	0.0123	0.0079

5. SUMMARY

The computationally efficient PE based on the WM has been proposed for complex signals. PE output is guaranteed to be positive, as desired for all applications requiring power estimation. Also, the PE can be designed to be predictive for delay sensitive control applications for which 5 < N < 21 is found adequate. Two optimum design methods have been derived, and of these the partial optimization method is of practical interest. In COSSAP software environment, the communication system simulations have been carried out to compare the behaviors of three controllers with or without PE. The results demonstrate obvious benefits of employing PE rather than power measurement when input SNR is low, and the advantage of using the partially-optimized PE over using the PE with conventional filters/predictors is clearly seen. In practice, an adaptive algorithm can be used to adjust the partially-optimized PE to suit for actual channel variation and SNR [6].

6. ACKNOWLEDGMENT

This project was financed by the Technology Development Centre of Finland (TEKES), Nokia Corporation, Telecom Finland, and Helsinki Telephone Company, Finland.

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8. APPENDICES

1. As stated in the text, $w_R(n) \sim (0, \sigma_w^2/2)$, $w_I(n) \sim (0, \sigma_w^2/2)$. The kurtosis of $w_R(n)$ or $w_I(n)$ is then $E\{w_R^4(n)\} = E\{w_I^4(n)\} = 3 \sigma_w^4/4$ [9]. The mean, variance and kurtosis of w(n) can be derived as

 $E\{|w(n)|^4\} = E\{w_R^4(n)\} + 2E\{w_R^2(n)\}E\{w_I^2(n)\} + E\{w_I^4(n)\} = 2\sigma_w^4.$

2. Equation (3) can be rewritten as $y(n) = \mathbf{h}^{T}\mathbf{S}\mathbf{h}$ where $\mathbf{S} = \mathbf{S}^{*T} = (\mathbf{x}+\mathbf{w})(\mathbf{x}+\mathbf{w})^{*T}$ is a Hermitian matrix. Taking the partial derivative of y(n) with respect to \mathbf{h} yields $\partial y(n)/\partial \mathbf{h} = (\mathbf{S}+\mathbf{S}^{*})\mathbf{h}$ [10]. Hence, the partial derivatives of the three terms in (6) can be derived as

$$\partial E\{y^{2}(n)\}/\partial \mathbf{h} = E\{2y(n)\cdot\partial y(n)/\partial \mathbf{h}\} = 2E\{(\mathbf{S}+\mathbf{S}^{*})\mathbf{h}\mathbf{h}^{T}\mathbf{S}\mathbf{h}\},\\ \partial E\{y(n)\cdot|\mathbf{x}(n+p)|^{2}\}/\partial \mathbf{h} = E\{|\mathbf{x}(n+p)|^{2}\cdot\partial y(n)/\partial \mathbf{h}\}\\ = E\{|\mathbf{x}(n+p)|^{2}\cdot(\mathbf{S}+\mathbf{S}^{*})\mathbf{h}\},\\ \partial E\{|\mathbf{x}(n+p)|^{4}\}/\partial \mathbf{h} = 0,$$

and (7) then stands.

3. Utilizing the equality $r(n) = \mathbf{h}^{\mathrm{T}}(\mathbf{x}+\mathbf{w}) = x(n+p)+\varepsilon(n)$, (4) and (5) can be further derived as

 $e(n) = x(n+p)\varepsilon^{*}(n) + x^{*}(n+p)\varepsilon(n) + \varepsilon(n)\varepsilon^{*}(n)$ = $2x_{\rho}(n+p)\varepsilon_{\rho}(n) + 2x_{\rho}(n+p)\varepsilon_{\rho}(n) + \varepsilon^{2}(n) + \varepsilon^{2}(n)$

$$= 2x_R(n+p)\varepsilon_R(n) + 2x_I(n+p)\varepsilon_I(n) + \varepsilon_R(n) + \varepsilon_I(n).$$

Bias = 4E{x_R(n+p)\varepsilon_R(n)}+2E{ $\varepsilon_R^2(n)$ }

$$= 4\mathbf{h}^{\mathrm{T}} E\{x_{R}(n+p) \cdot \mathbf{x}_{R}\} - 4E\{x_{R}(n+p) \cdot x_{R}(n+p)\} + 2E\{\varepsilon_{R}^{2}(n)\}$$

= 4[\mathbf{h}^{\mathrm{T}}\mathbf{r}_{xR} - \mathbf{R}_{x}(0)/2] + 2E\{\varepsilon_{R}^{2}(n)\} (A.1)

The first equality in (A.1) stands because of the equal-statistics assumptions on $w_R(n)$ and $w_I(n)$, and on $x_R(n)$ and $x_I(n)$. The second equality stands since $w_R(n)$ is a zero-mean Gaussian process. The last quality stands due to the definitions of \mathbf{r}_{xR} and $R_R(0)$ in Section 3.2. In the case of using Wiener filters, replacing \mathbf{h} by \mathbf{h}_{opt} , replacing $E\{\varepsilon_R^2(n)\}$ by $E\{\varepsilon_R^2(n)\}_{min}$, utilizing (11) yields (12).